

# FEniCS at KTH: projects, challenges and future plans

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# Overview

- FEniCS at KTH today
- A FEniCS prototype
- Ongoing projects
- Challenges
- Future plans

# FEniCS at KTH today

- JH + JJ + 1 PhD + 3 MSc
- Dag Lindbo/Gunilla Kreiss - 2-phase flow/level set
- 1 PhD/Anders Szepessy - Hamilton Jacobi eqns.
- 1 PhD/Dan Henningsson (JH) - transition
- 1 MSc/Luca Brandt (JH) - optimal disturbances
- Gustav Amberg group (Femlego) - testing
- MSc FEM course (JH) - Puffin ( $\rightarrow$  Dolfin/FFC/FIAT)
- MSc CFD project course (JJ?) - Dolfin/FFC/FIAT
- Wide general interest in the project

# TACO - Techn. for Advanced Comp.

- Johan Hoffman
- Johan Jansson
- Murtazo Nazarov (PhD): compressible turbulence
- Oana Marin (MSc): free surface flow, level sets
- Alessio Quaglino (MSc): large def. solid mech., contact
- Michael Stöckli (MSc): fluid-structure, ALE

# TACO - Techn. for Advanced Comp.

TACO projects today:

- G2: turbulent flow in complex geometries
- G2: friction bc for turbulent flow
- G2: thermodynamics (turbulent compressible flow)
- Mesh refinement/coarsening/smoothing/flipping/...
- Free surface flow/level set
- ALE fluid structure interaction
- Large deformation structure mechanics/contact

# A FEniCS prototype

Vision of FEniCS: automation of

- discretization: done?
- discrete solver
- adaptivity/error control
- modeling
- optimization

# A FEniCS prototype

Vision: Automation of

- discretization:
  1. DE → Form: not done?
  2. Form → element matrix: FFC/FIAT
- discrete solver: not done?
- adaptivity/error control: not done?
- modeling: not done?
- optimization: not done?

# A FEniCS prototype

FEniCS prototype for turbulent flow: Dolfin NSE solver

- discretization:
  1. DE → Form: General Galerkin G2
  2. Form → element matrix: FFC/FIAT
- discrete solver: not done (PETSc + MG)
- adaptivity/error control: mesh refinement based on output error control by duality.
- turbulence modeling: G2
- optimization: not done

# Navier-Stokes Equations (NSE)

$$R(\hat{u}) = \begin{pmatrix} \dot{u} + u \cdot \nabla u - \nu \Delta u + \nabla p - f \\ \nabla \cdot u \end{pmatrix} = 0$$

$\hat{u} = (u, p)$ :  $u$  velocity,  $p$  pressure,  $\nu$  viscosity,  $f = 0$

- Pointwise existence & uniqueness unknown:  $R(\hat{u}) = 0$   
(Clay Institute \$1 million Prize Problem)
- Existence (but not uniq.) of weak solution (Leray 1934):

Find  $\hat{u} \in \hat{V}$  :  $(R(\hat{u}), \hat{v}) = 0 \quad \forall \hat{v} = (v, q) \in \hat{V}$

$$(R(\hat{u}), \hat{v}) \equiv (\dot{u}, v) + (u \cdot \nabla u, v) - (\nabla \cdot v, p) + (\nabla \cdot u, q) + (\nu \nabla u, \nabla v)$$

$$\hat{V} \subset H^1(Q), Q = \Omega \times I, (v, w)_Q \equiv \int_Q v \cdot w \, dxdt$$

# Turbulent incompressible flow

Typical scientific goals of today:

- Prove exist & uniq of pointwise NSE:  $R(\hat{u}) = 0$
- Push limit of DNS (wrt  $Re^3$  constraint,  $Re = UL/\nu$ )
- Turbulence modeling: find model for unresolved scales  
(filtering of NSE: Reynolds stresses, closure problem)

Alternative scientific goals:

- Approximate weak solution  $\hat{U}$ : weak uniqueness in  
(mean value) output  $M(\hat{U})$ : stability of  $\hat{U}$  wrt  $M(\cdot)$
- Adaptive algorithm:  $\min \#dof : error(M(\hat{U})) < TOL$

# Existence of $\epsilon$ -Weak Solutions

- $W_\epsilon = \{\hat{u} \in \hat{V} : |(R(\hat{u}), \hat{v})| \leq \epsilon \|\hat{v}\|_{\hat{V}} \quad \forall \hat{v} \in \hat{V} \subset H^1\}$   
(approximate weak solution:  $\sim \|R(\hat{u})\|_{H^{-1}} \leq \epsilon$ )
- Existence: Construction of  $W_\epsilon$ : General Galerkin G2
- Find  $\hat{U} \in \hat{V}_h$ :  $(R(\hat{U}), \hat{v}) + (hR(\hat{U}), R(\hat{v})) = 0 \quad \forall \hat{v} \in \hat{V}_h$

$$\frac{1}{2} \|U(t)\|^2 + \|\sqrt{\nu} \nabla U\|_Q^2 + \|\sqrt{h} R(\hat{U})\|_Q^2 = \frac{1}{2} \|U(0)\|^2$$

$$\begin{aligned} (R(\hat{U}), \hat{v}) &= (R(\hat{U}), \hat{v} - \pi_h \hat{v}) - (hR(\hat{U}), R(\pi_h \hat{v})) \\ &\leq (C + M_U) \|hR(\hat{U})\|_Q \|\hat{v}\|_{\hat{V}} \leq C\sqrt{h} \|\hat{v}\|_{\hat{V}} \end{aligned}$$

- $\hat{U} \in \mathbf{G2} \Rightarrow \hat{U} \in W_\epsilon \quad \epsilon = (C + M_U) \|hR(\hat{U})\|_Q$

# Weak Uniqueness: Duality

- Output (functional):  $M(\hat{u}) \equiv (\hat{u}, \hat{\psi})$  (e.g. drag or lift)

- ## ■ Adjoint Navier-Stokes equations (given by NSE):

**Find**  $\hat{\varphi} = (\varphi, \theta)$  :  $a(\hat{u}, \hat{w}; \hat{v}, \hat{\varphi}) = M(\hat{v}) \quad \forall \hat{v} = (v, q) \in \hat{V}$

$$a(\hat{u}, \hat{w}; \hat{v}, \hat{\varphi}) \equiv (\dot{v}, \varphi) + (u \cdot \nabla v, \varphi) + (v \cdot \nabla w, \varphi) \\ - (\nabla \cdot \varphi, q) + (\nabla \cdot v, \theta) + (\nu \nabla v, \nabla \varphi)$$

- Weak Uniqueness:  $\hat{u}, \hat{w} \in W_\epsilon$ ,  $S_\epsilon(\hat{\psi}) \equiv \max_{\hat{u}, \hat{w} \in W_\epsilon} \|\hat{\varphi}\|_{\hat{V}}$

$$\begin{aligned} |M(\hat{u}) - M(\hat{w})| &= |a(\hat{u}, \hat{w}; \hat{u} - \hat{w}, \hat{\varphi})| \\ &= |(R(\hat{u}), \hat{\varphi}) - (R(\hat{w}), \hat{\varphi})| \leq 2\epsilon S_\epsilon(\hat{\psi}) \end{aligned}$$

- Exact solution ( $\epsilon = 0$ ): stability information lost!

# Weak Uniqueness: Duality

- Weak Uniqueness:  $\hat{u}, \hat{w} \in W_\epsilon$

$$|M(\hat{u}) - M(\hat{w})| \leq 2\epsilon S_\epsilon(\hat{\psi}) \quad \|R(\hat{u})\|_{H^{-1}}, \|R(\hat{w})\|_{H^{-1}} \leq \epsilon$$

- Computability:  $\hat{u} \in W_\epsilon$  and  $\hat{U} \in G2$

$$|M(\hat{u}) - M(\hat{U})| \leq (\epsilon + \epsilon_{G2}) S_{\epsilon_{G2}}(\hat{\psi}) \quad \epsilon_{G2} = C \|hR(\hat{U})\|$$

- Residual only needs to be small in a weak norm!!!  
(for weak uniqueness)

- $\|R(\hat{u})\|_{H^{-1}}$  &  $\|hR(\hat{U})\|_{L_2}$  vs  $\|R(\hat{u})\|_{L_2}$

- Weak uniqueness characterized by stability factor  $S_\epsilon(\hat{\psi})$

# Automation of turbulence simulation

NSE:  $R(\hat{u}) = 0$

G2:  $\hat{U} \in \hat{V}_h : (R(\hat{U}), \hat{v}) + SD_\delta(\hat{U}; \hat{v}) = 0 \quad \forall \hat{v} \in \hat{V}_h$

Functional output:  $M(\hat{u}) = (\hat{u}, \hat{\psi})$  (drag, lift,...)

$$|M(\hat{u}) - M(\hat{U})| = |a(\hat{u}, \hat{U}; \hat{u} - \hat{U}, \hat{\varphi})| = |(R(\hat{u}), \hat{\varphi}) - (R(\hat{U}), \hat{\varphi})|$$

$$\leq \epsilon S_\epsilon + |(R(\hat{U}), \hat{\varphi})| = \epsilon S_\epsilon + |(R(\hat{U}), \hat{\varphi} - \hat{\Phi}) + SD_\delta(\hat{U}; \hat{\Phi})|$$

for all  $\hat{\Phi} \in \hat{V}_h$ , in particular for the interpolant of  $\hat{\varphi}^h$  in  $\hat{V}_h$

Use interpolation estimates:  $\|h^{-1}(\hat{\varphi} - \hat{\varphi}^h)\| \leq C_i \|\hat{\varphi}\|_1$

Compute (using G2) approx. dual solution  $\hat{\varphi}_h = (\varphi_h, \theta_h)$

# Automation of turbulence simulation

- G2 for NSE: No filtering. No Reynolds stresses.  
G2 automatic “turbulence model”.
- Adaptive algorithm captures separation points, and  
“correct” (finite limit) dissipation in the turbulent wake.
- Mean value output (drag, lift, frequencies, separation  
points, pressure coeff,...) computable up to a tolerance  
corresponding to experimental accuracy ( $\approx 1\text{-}5\%$ ).
- About 10-100 times less mesh points needed to  
compute drag than in non-adaptive LES.
- Simple/complex geometry: laptop/cluster.

# Automation of turbulence simulation

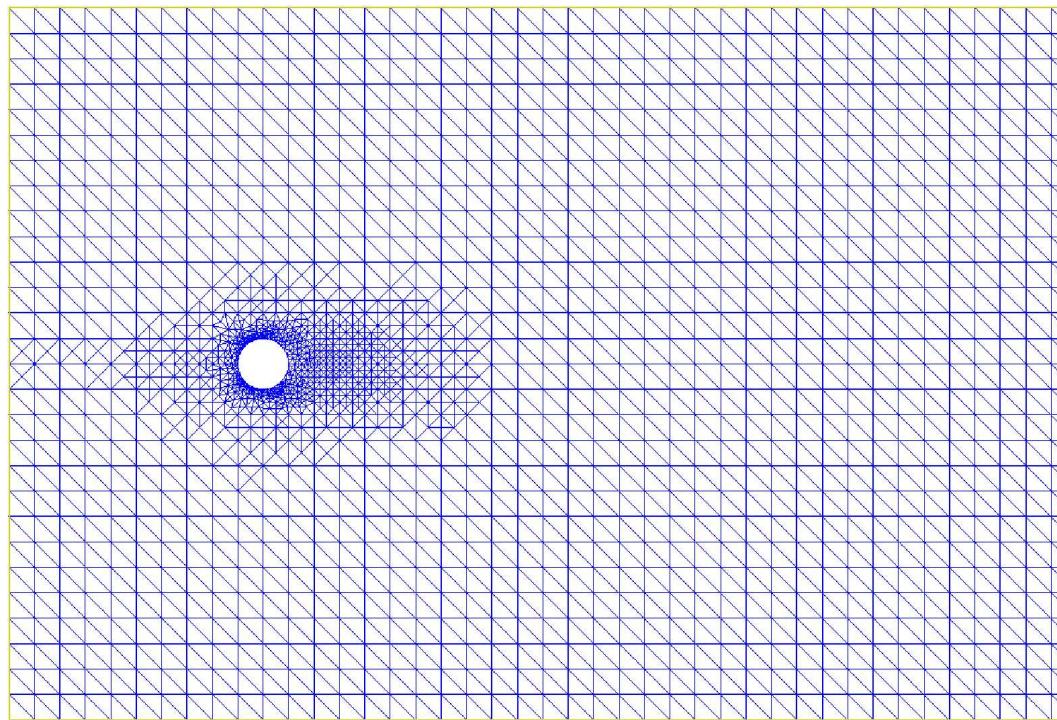
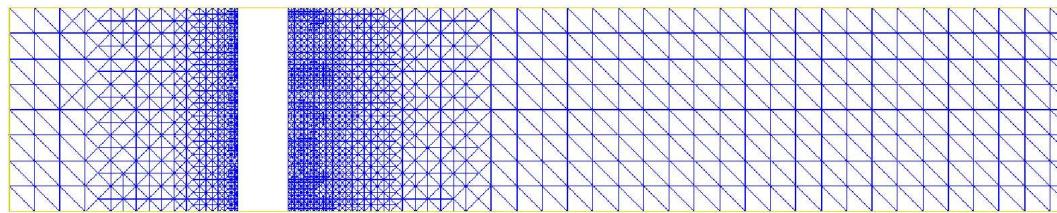
$$|M(\hat{u}) - M(\hat{U})| \leq \sum_{K \in \mathcal{T}} \mathcal{E}_K = \sum_{K \in \mathcal{T}} \|hR(\hat{U})\| \|\hat{\varphi}_h\|_1 + |SD_\delta(\hat{U}; \hat{\varphi}_h)|$$

Galerkin discretization error + stabilization modeling error

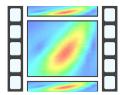
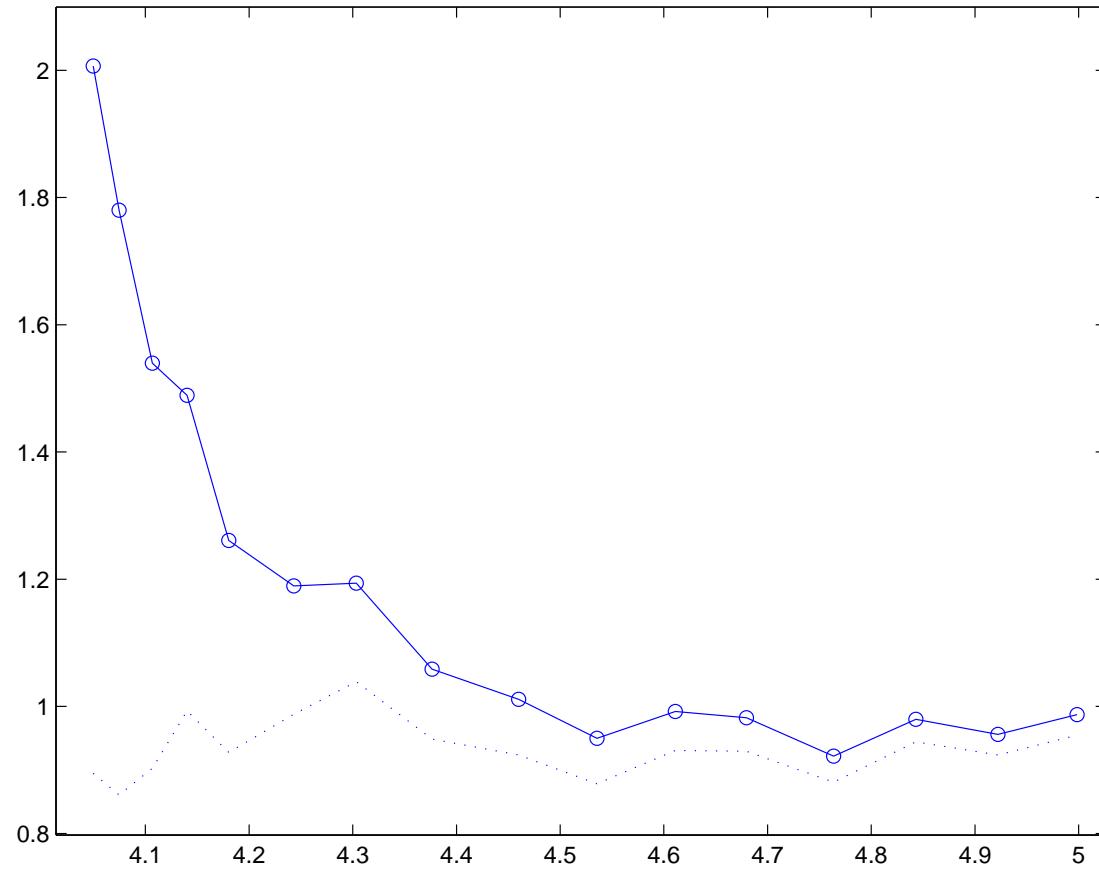
Adaptive algorithm: From coarse mesh  $\mathcal{T}^0$  do

- (1) compute primal and dual problem on  $\mathcal{T}^k$
- (2) if  $\sum_{K \in \mathcal{T}^k} \mathcal{E}_K^k < \text{TOL}$  then STOP, else
- (3) refine elements  $K \in \mathcal{T}^k$  with largest  $\mathcal{E}_K^k \rightarrow \mathcal{T}^{k+1}$
- (4) set  $k = k + 1$ , then goto (1)

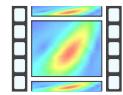
# Ref. Mesh wrt $c_D$ : circular cylinder



# Circular cylinder: $c_D \approx 1.0$

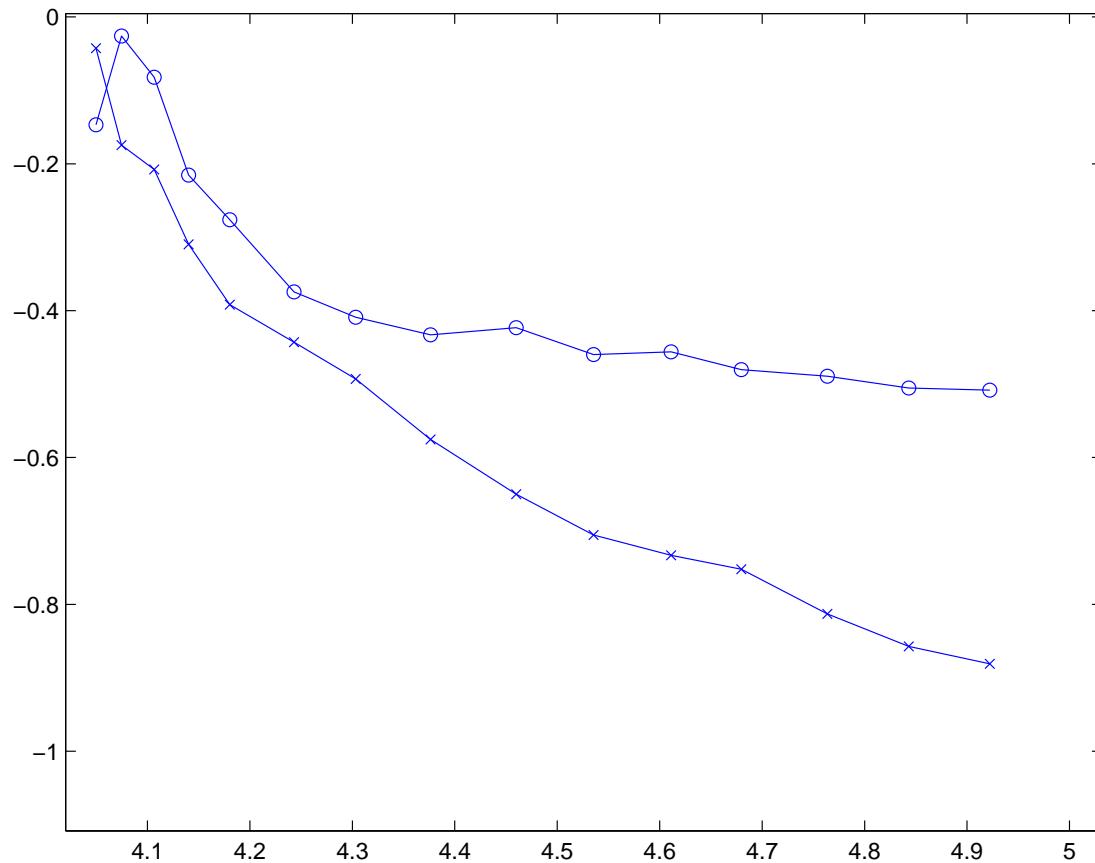


*circular cylinder*

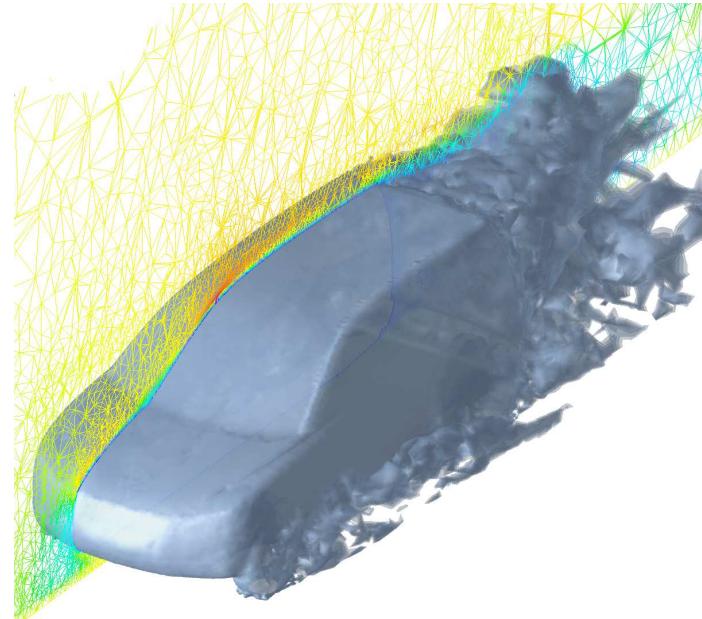
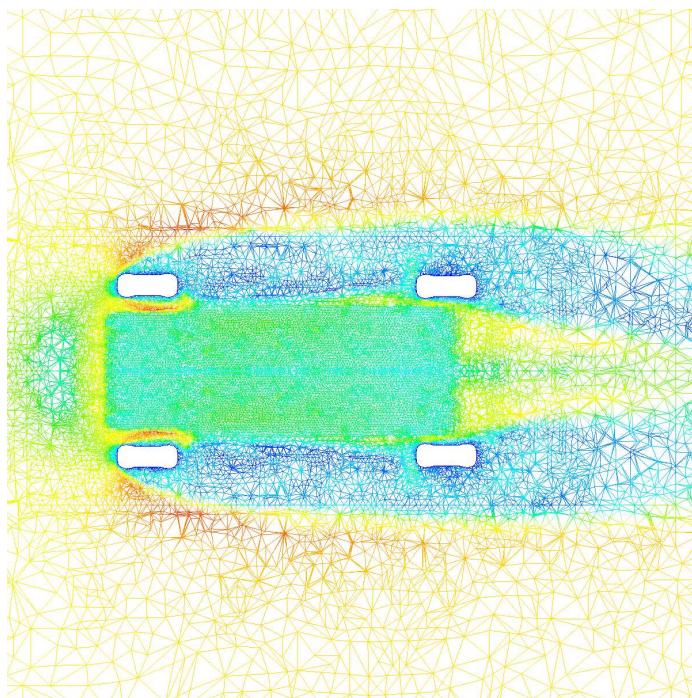
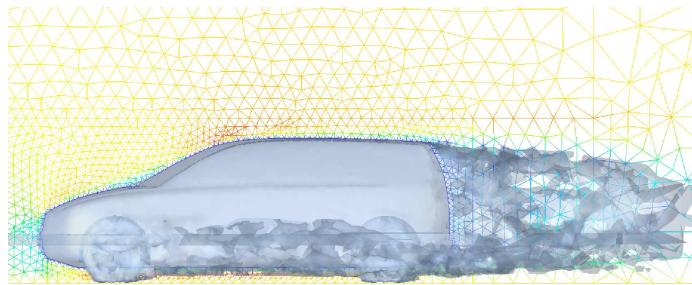


*dual solution*

# Circular cylinder: error estimates



# G2 for complex geometry (Volvo CC)

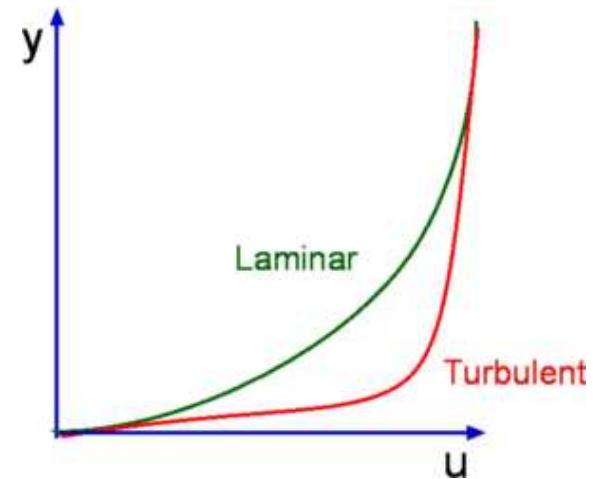
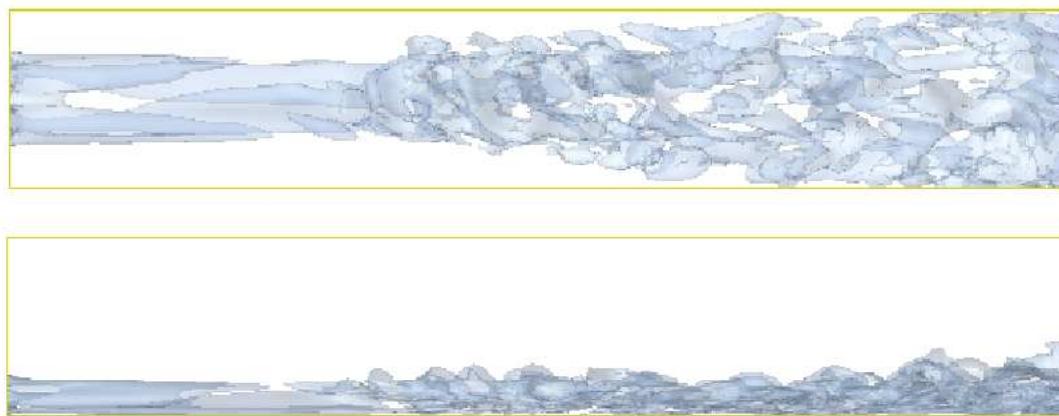


# Turbulent boundary layers

No slip boundary conditions ok for modeling laminar boundary layers.

For high  $Re$  boundary layer undergoes transition.

Extremely expensive to resolve turbulent boundary layer:  
We need wall-model for correct separation and skin friction



# Turbulent boundary layers

Experiments: boundary skin friction  $c_f \sim Re^{-0.2}$

That is: no Law of finite dissipation for  $c_f$ !

Skin friction  $c_f$  depend on  $Re$ !

Cannot expect skin friction to be mesh independent:

We have to resolve/model the turbulent boundary layer!  
(unless  $c_f \approx 0!!$ )

# Skin friction boundary condition

Slip with friction boundary condition [Maxwell, Navier,...]

Friction coefficient  $\beta$ ;  $\beta = 0$ : slip b.c.,  $\beta = \infty$ : no slip b.c.

[LES + Boundary Layer theory: Layton, John, Iliescu,...]

Simple wall model:  $\beta \sim c_f$  (skin friction  $c_f \sim Re^{-0.2}$ )

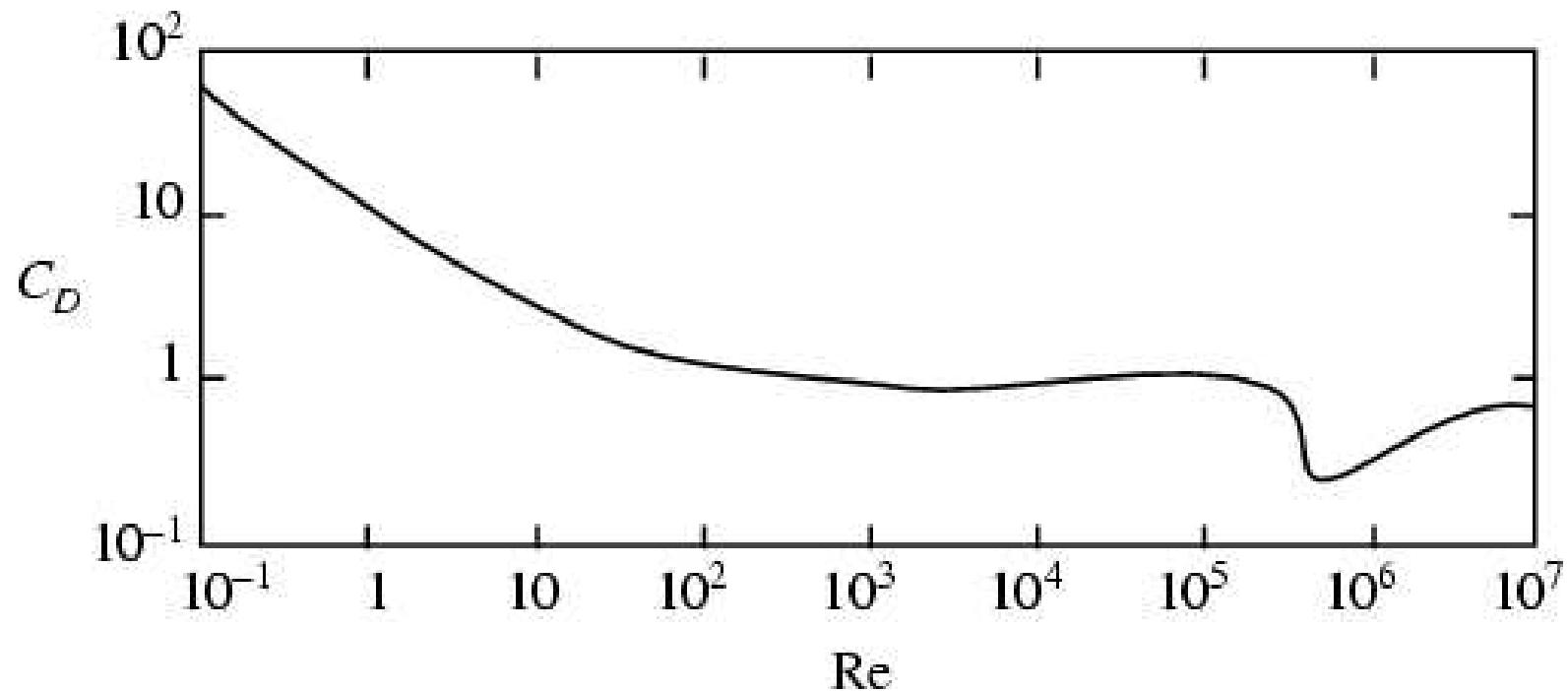
$$\beta = \beta(Re, h); \lim_{h \rightarrow 0} \beta = \infty, \lim_{Re \rightarrow \infty} \beta = 0$$

$$\frac{1}{2} \|U(t)\|^2 + \sum_{i=1}^2 \|\sqrt{\beta} u \cdot \tau_i\|_{\Gamma \times I}^2 + \|\sqrt{h} R(\hat{U})\|_Q^2 = \frac{1}{2} \|U(0)\|^2$$

(with  $\nu$  small)

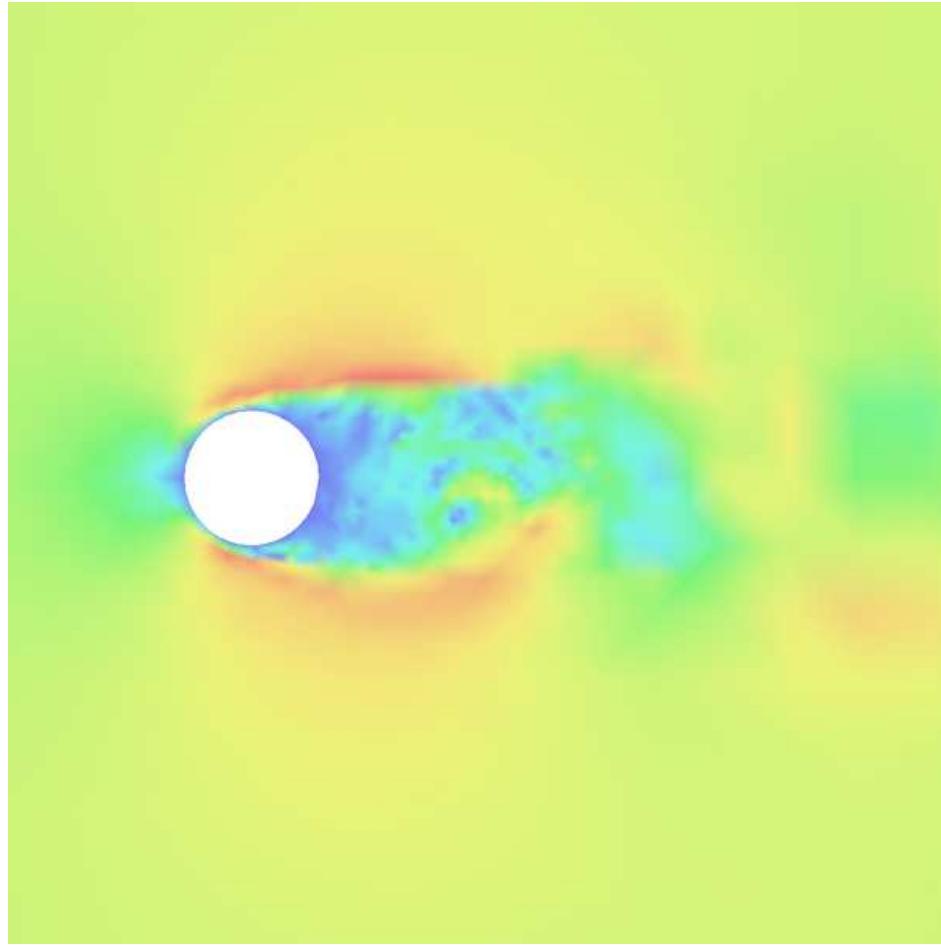
# Drag crisis for a cylinder

Turb. boundary layer  $\Rightarrow$  high momentum near boundary  $\Rightarrow$   
delayed separation  $\Rightarrow$  small wake  $\Rightarrow$  drag crisis

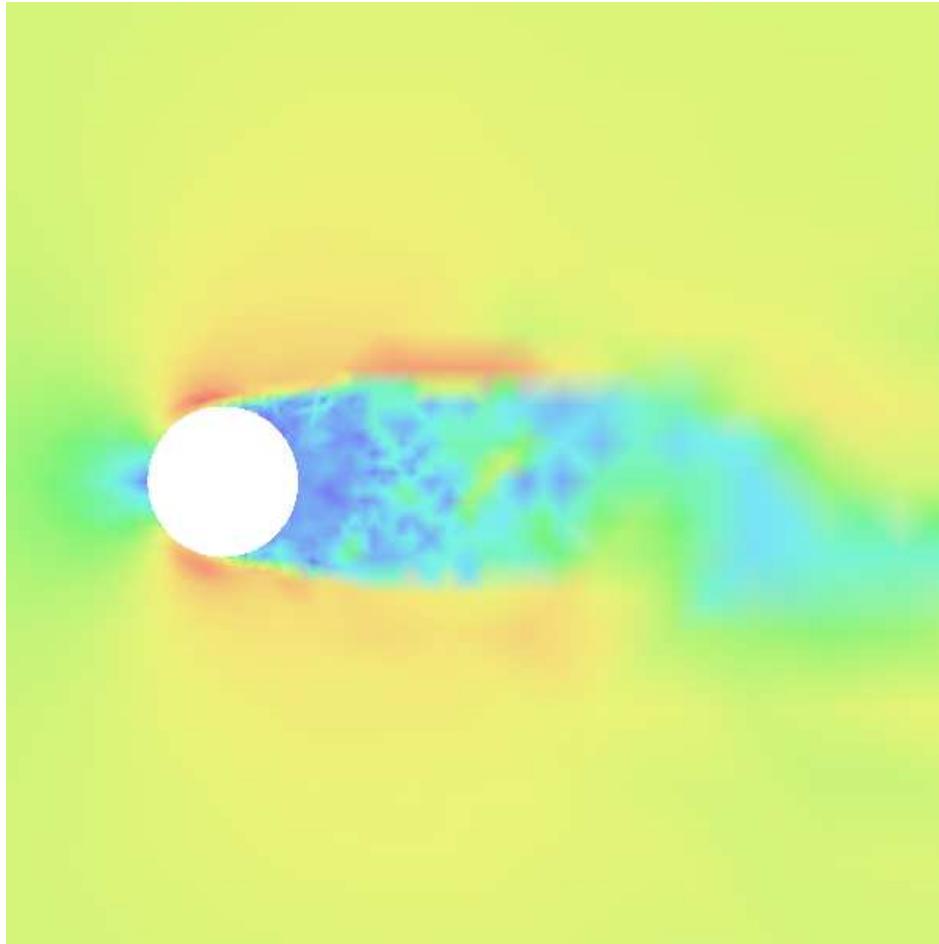


Drag crisis for a circular cylinder at  $Re \sim 10^5 - 10^6$

drag crisis;  $\beta = 1$ :  $c_D \approx 1.0$



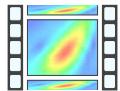
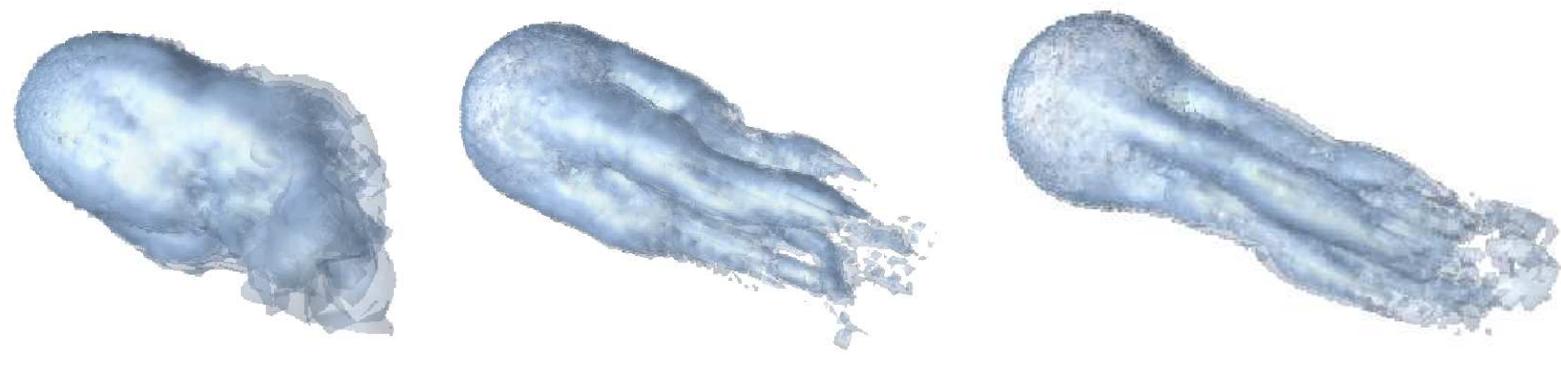
drag crisis;  $\beta = 2 \times 10^{-2}$ :  $c_D \approx 0.7$



**drag crisis:**  $\beta = 1 \times 10^{-2}$ ;  $c_D \approx 0.5$

drag crisis;  $\beta = 5 \times 10^{-3}$ :  $c_D \approx 0.45$

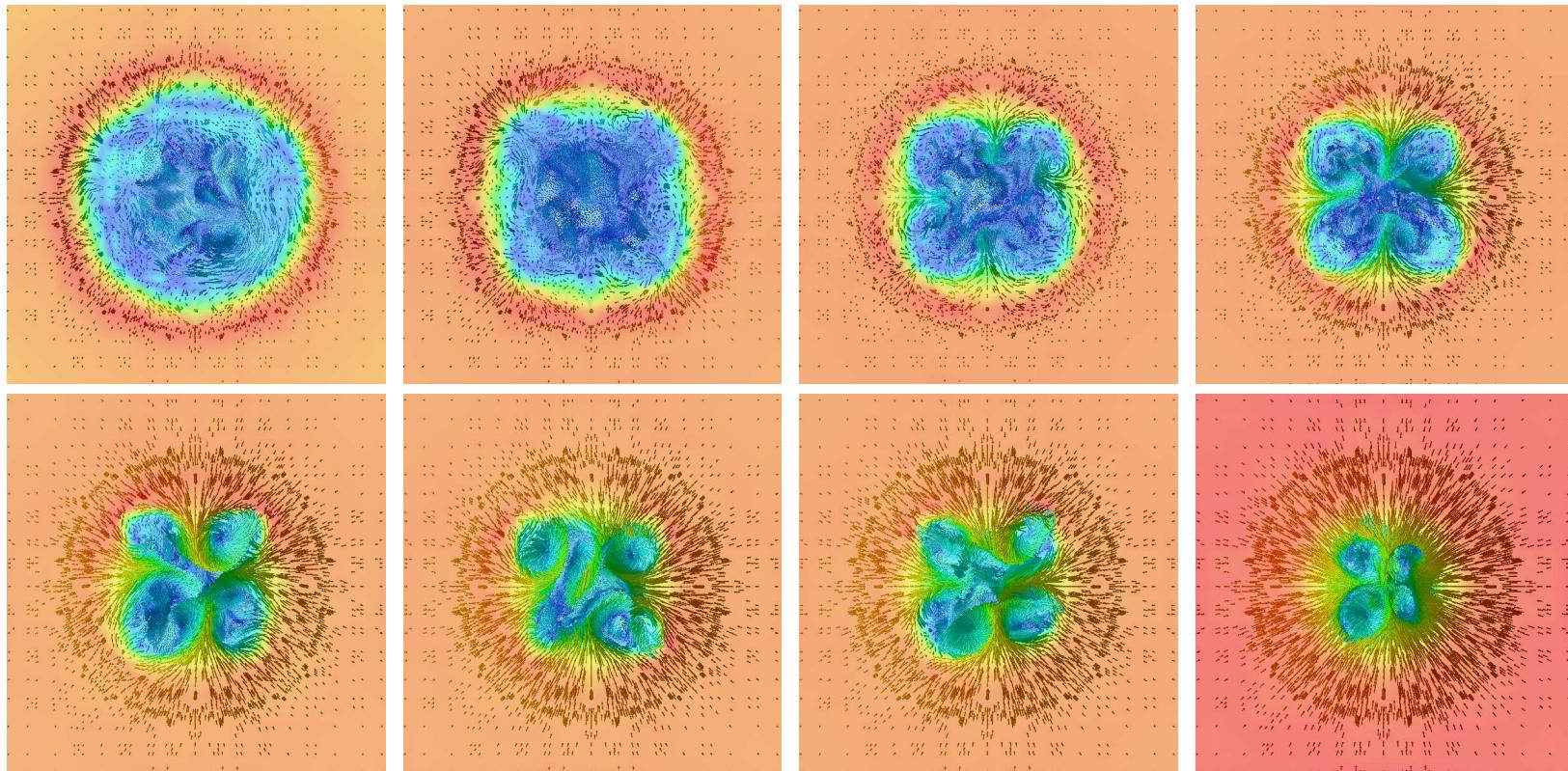
# Drag crisis for a sphere



# Modeling of drag crisis for a sphere by skin friction model

**Friction coeff.**  $\beta = 0.1 \rightarrow 0.01$  :  $c_D = 0.4 \rightarrow 0.2$

# Drag crisis for a sphere

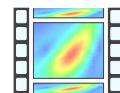
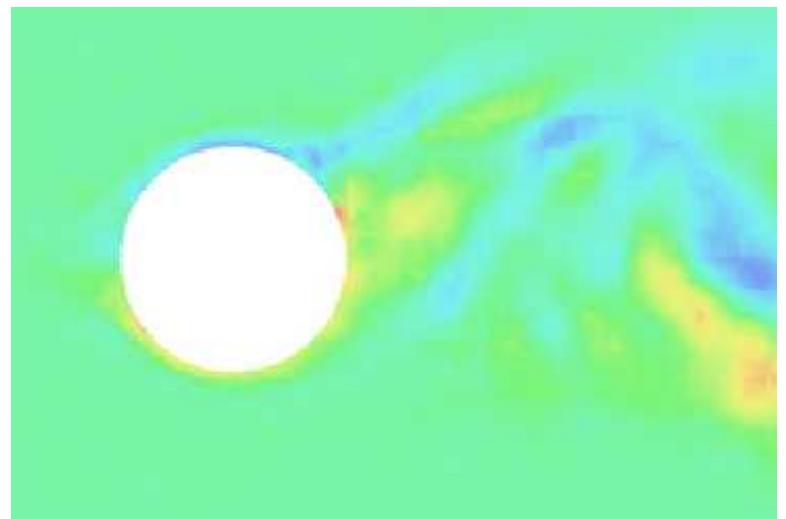
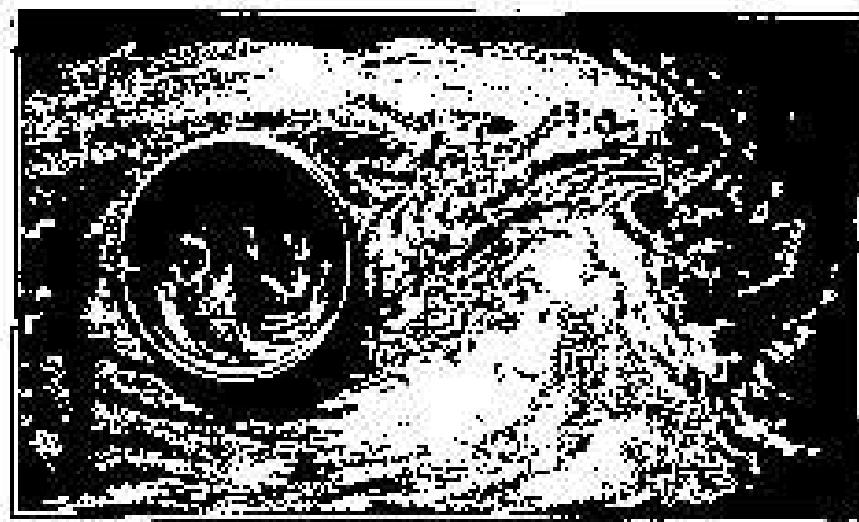


# EG2 and Turbulent Euler solutions

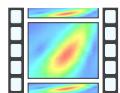
$\beta \rightarrow 0; Re \rightarrow \infty (\nu \rightarrow 0) \Rightarrow$  Euler/G2 + slip b.c. (EG2)

EG2: no empirical parameters; only  $h$  (very general...)

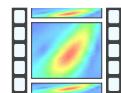
No experimental results for cylinder at  $Re > 10^7$



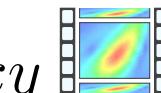
$u$



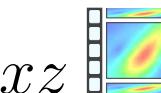
$p$



$\omega_1, xy$

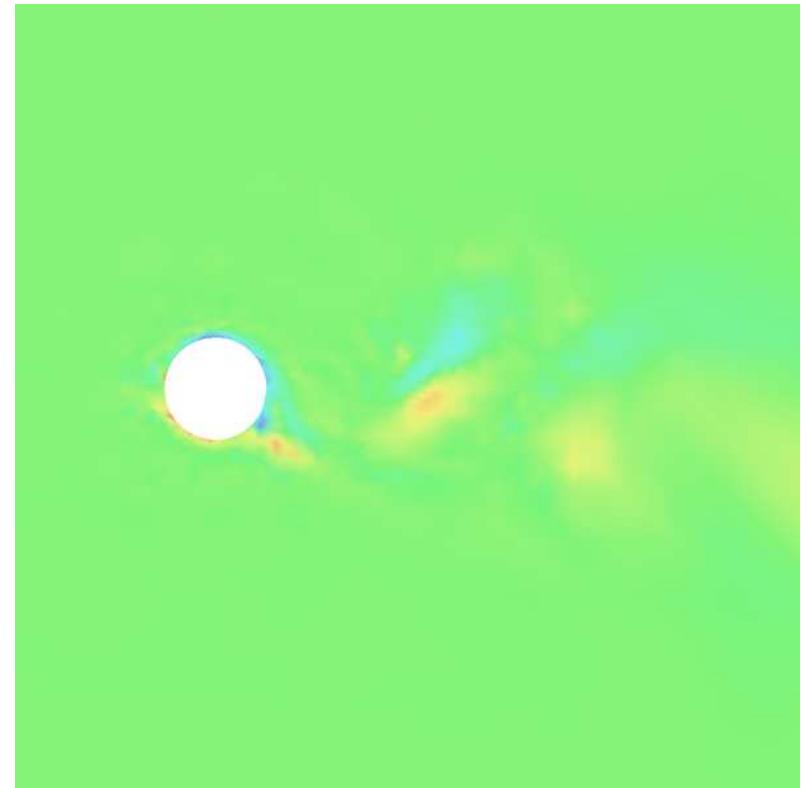


$\omega_1, xz$



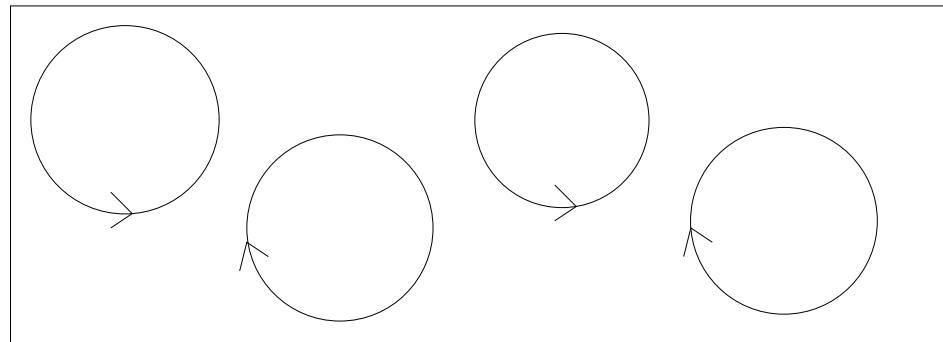
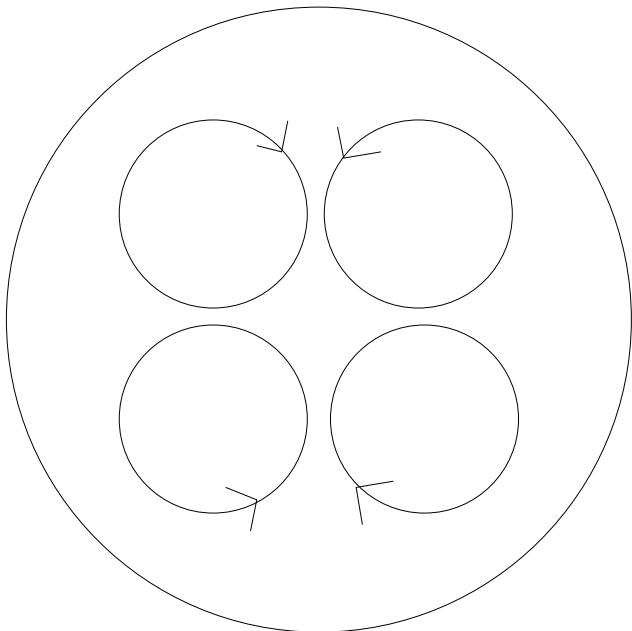
$\omega_1, yz$

# EG2 and Turbulent Euler solutions



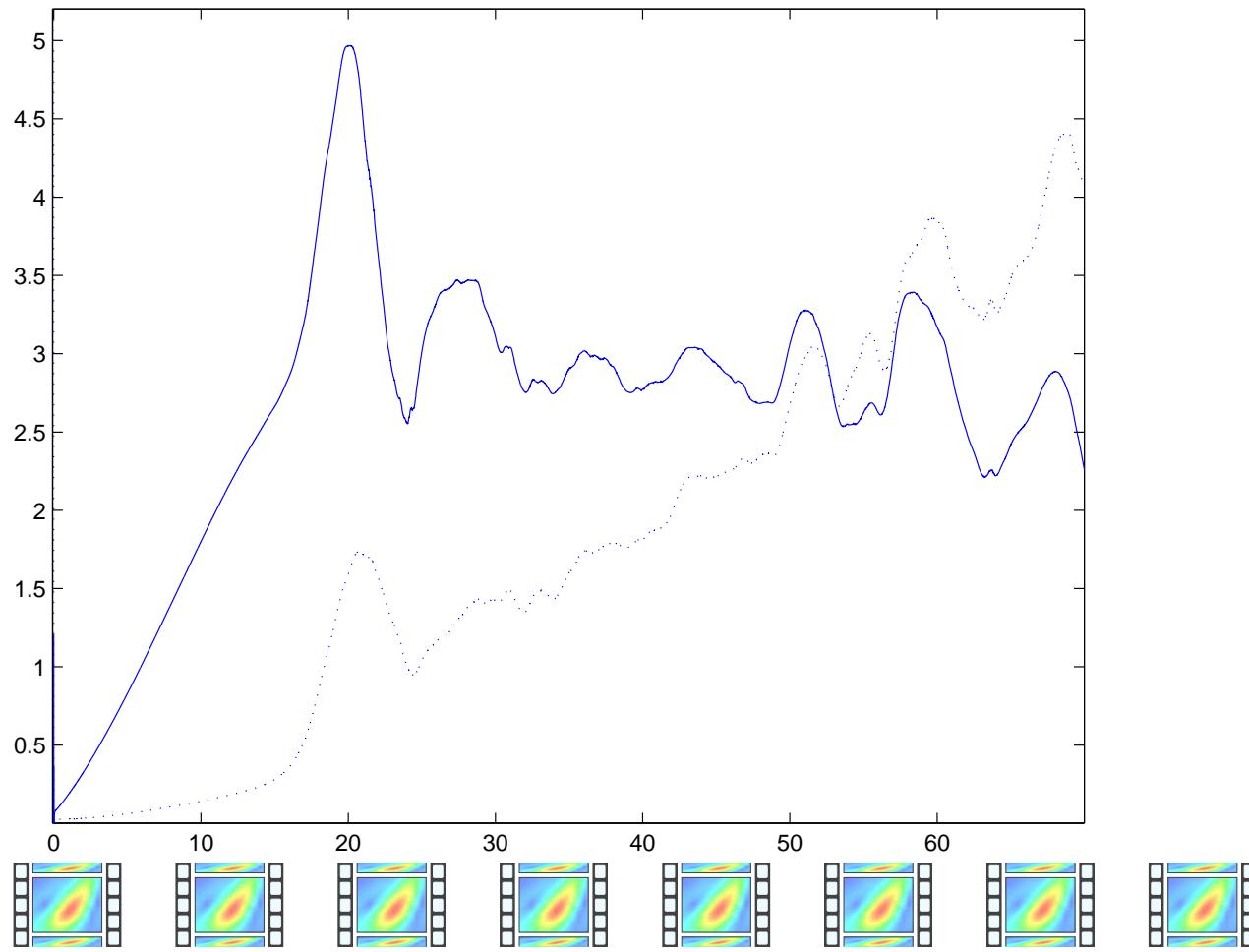
Euler relevant for very large  $Re$ : geophysical flow!

# EG2 solutions: sphere and cylinder



EG2 solutions of physical relevance for (very) high  $Re$ ?

# Simulation of take-off: lift vs drag



# Turbulent Compressible Flow

EG2 for the compressible Euler equations:

- Conservation of total mass, momentum, and energy
- Automatic satisfaction of 2nd Law.

$$\dot{\rho} + \nabla \cdot (u\rho) = 0$$

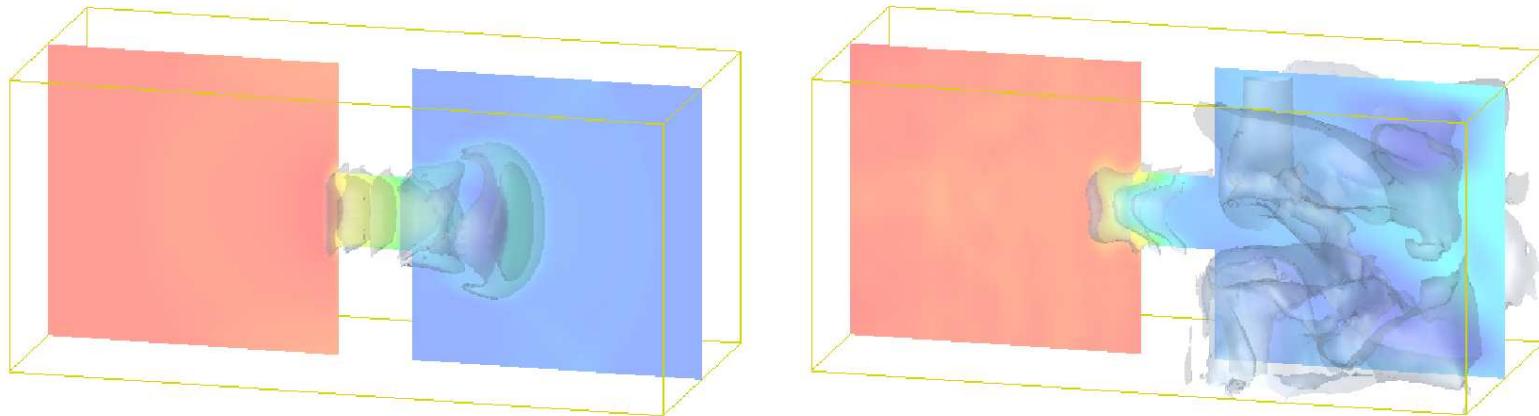
$$\dot{m} + \nabla \cdot (um) + \nabla p = 0$$

$$\dot{e} + \nabla \cdot (ue) + \nabla \cdot (up) = 0$$

# Turbulent Compressible Flow

EG2 for the compressible Euler equations:

- Conservation of total mass, momentum, and energy
- Automatic satisfaction of 2nd Law.

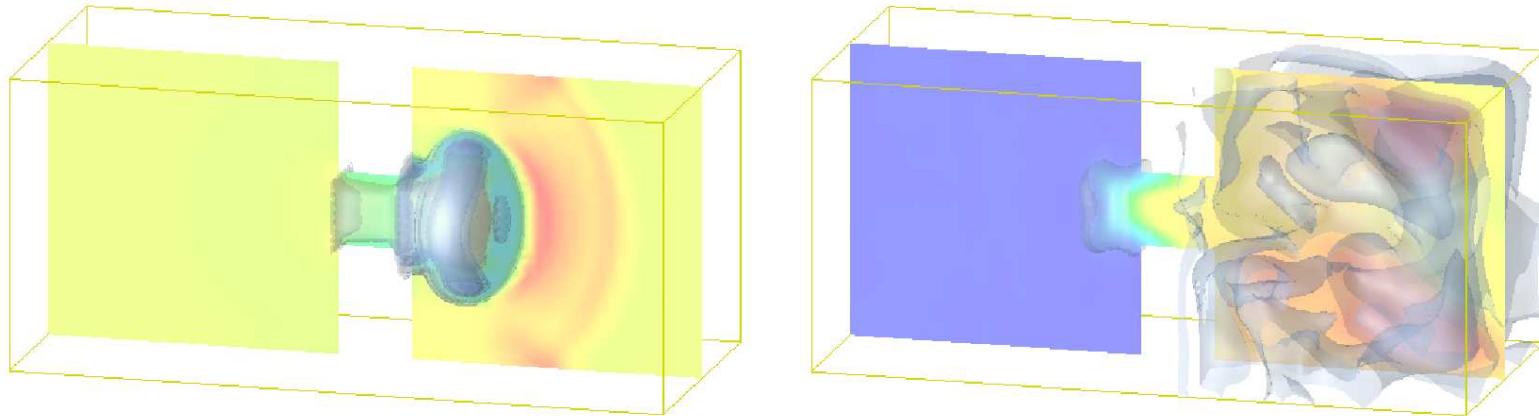


Density

# Turbulent Compressible Flow

EG2 for the compressible Euler equations:

- Conservation of total mass, momentum, and energy
- Automatic satisfaction of 2nd Law.

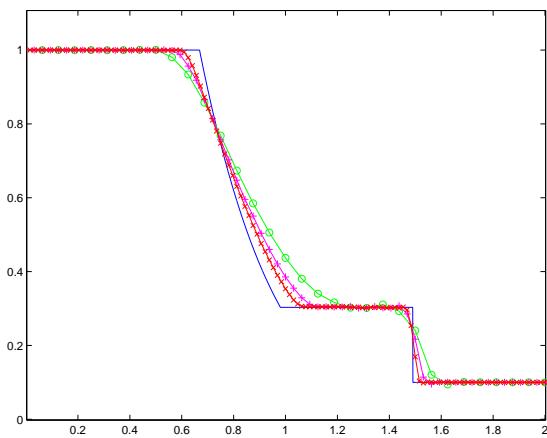
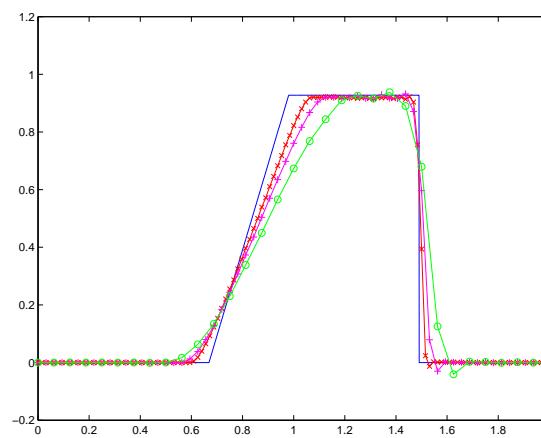
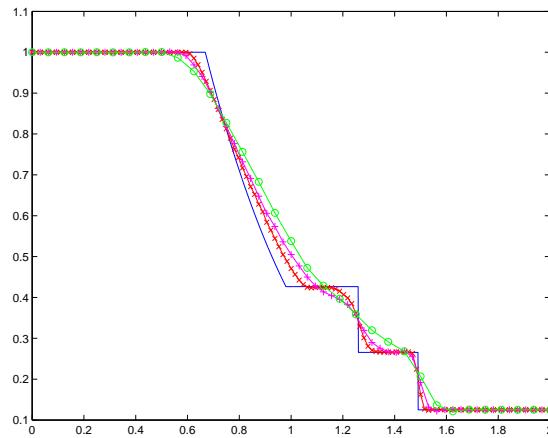


Temperature

# Turbulent Compressible Flow

EG2 for the compressible Euler equations:

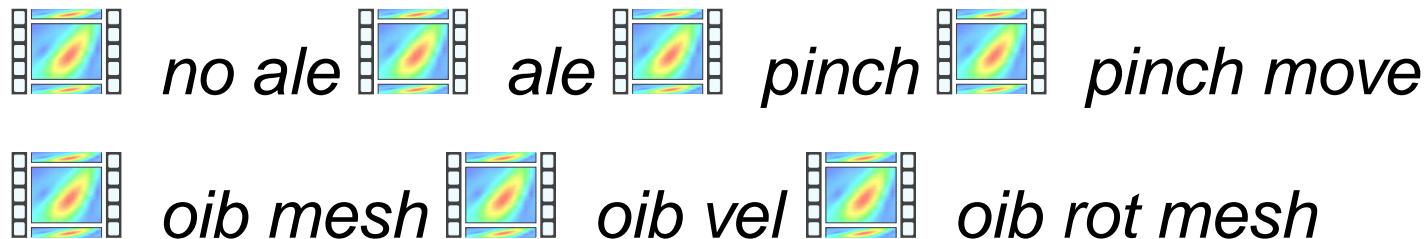
- Conservation of total mass, momentum, and energy
- Automatic satisfaction of 2nd Law.



Shocktube on coarse meshes: density, velocity, pressure

# Fluid-structure: ALE

- Ex: blood flow with elastic walls,...
- ALE: mesh moving/smoothing, object in a box,...
- Splitting of discrete system: NS + Ko
- Turbulence, transition, separation,...
- Adaptivity: moving domain, splitting, h-p-r,...



# Mesh algorithms

- Mesh refinement/coarsening
- Mesh smoothing (Laplacian, optimization,...)
- Edge flip/face swap
- Local remesh
- Projection between general meshes
- Hierarchy vs. one mesh
- GMG vs. AMG
- Optimal alg. vs. simple alg. + smooth/flip/swap

# Mesh refinement

Goals for (tetrahedral) mesh refinement:

1. cut edges (reduce  $h$ )
  2. avoid adding edges to node (avoid small angles)
  3. avoid hanging nodes (localization)
- 
- Edge vertex insertion (1 0 1)
  - Face vertex insertion (0 0 1)
  - Cell vertex insertion (0 0 1)
  - Uniform cell refinement (1 1 0)

# Mesh coarsening

Goals for (tetrahedral) mesh coarsening:

1. increase  $h$
2. avoid adding edges to node (avoid small angles)
3. localization
  - Edge collapse
  - Face collapse
  - Cell collapse

Alt. 1: coarsen by mesh hierarchy (use parent-child info).  
Alt. 2: coarsen by “Matt-algorithm”.

# Free surface flow - level sets

Applications: dam break, flow past structures, ships,...

Challenges: topology changes, turbulence, wetting bc,...

Method: G2, variable density/viscosity, “level set”,...

# Large deformation - contact

Physics engine for animation using Ko/DOLFIN/FFC/FIAT

Industrial partner: plug-in for gaming, simulators,...

Real-time: efficiency, contact model,...

# FEniCS - Challenges

## Challenges

- Dolfin module developers - need stable kernel
- New users - simple build (including dependencies)
- Industrial partners (including software companies)

## Solutions

- dolfin-dev + dolfin-stable
- scons/cmake/?
- A license that does not exclude industrial partners

# Expected input to FEniCS

- Automation of modeling: turbulent flow (G2)
- Mesh algorithms: refine/coarse/smooth/flip/...
- General function projections
- Modules: turbulence, free surface, ale, solid, contact,...
- Advanced modules/top applications
  - new abstractions, users/developers, visibility,...
- New developers → testing, contribution,...
- Use in education → visibility, testing,...
- Industrial partners → visibility, testing, funded devel.,...

# Future plans

FEniCS prototype: automation of

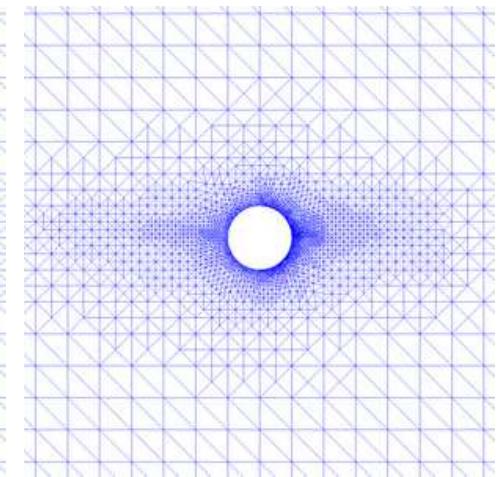
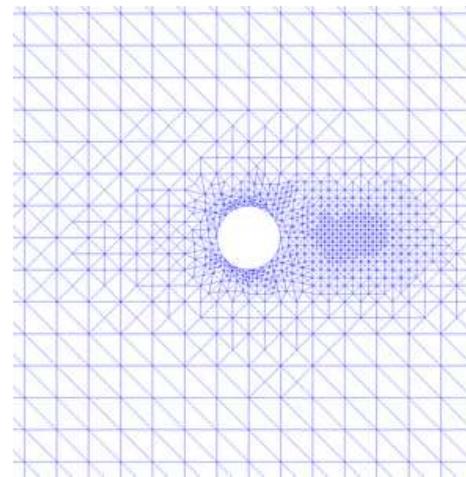
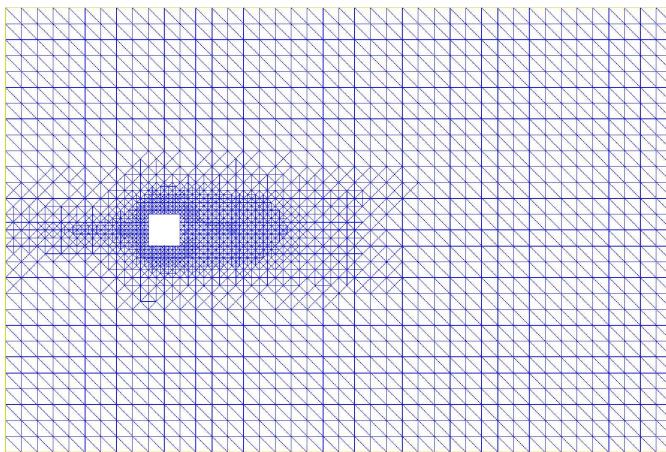
- turbulent incompressible/compressible flow,
- fluid-structure interaction,
- general free-surface problem,
- h-p-r adaptivity.

# G2 - automation of discretization

General Galerkin G2: Find  $\hat{U} \in \hat{V}_h \subset \hat{V}$ :

$$(R(\hat{U}), \hat{v}) + (hR(\hat{U}), R(\hat{v})) = 0 \quad \forall \hat{v} \in \hat{V}_h$$

The G2 solution  $\hat{U} \in \hat{V}_h$  is defined on a computational mesh, of size  $h(x)$ , which defines a smallest scale.



# G2 - automation of discretization

General Galerkin G2: Find  $\hat{U} \in \hat{V}_h \subset \hat{V}$ :

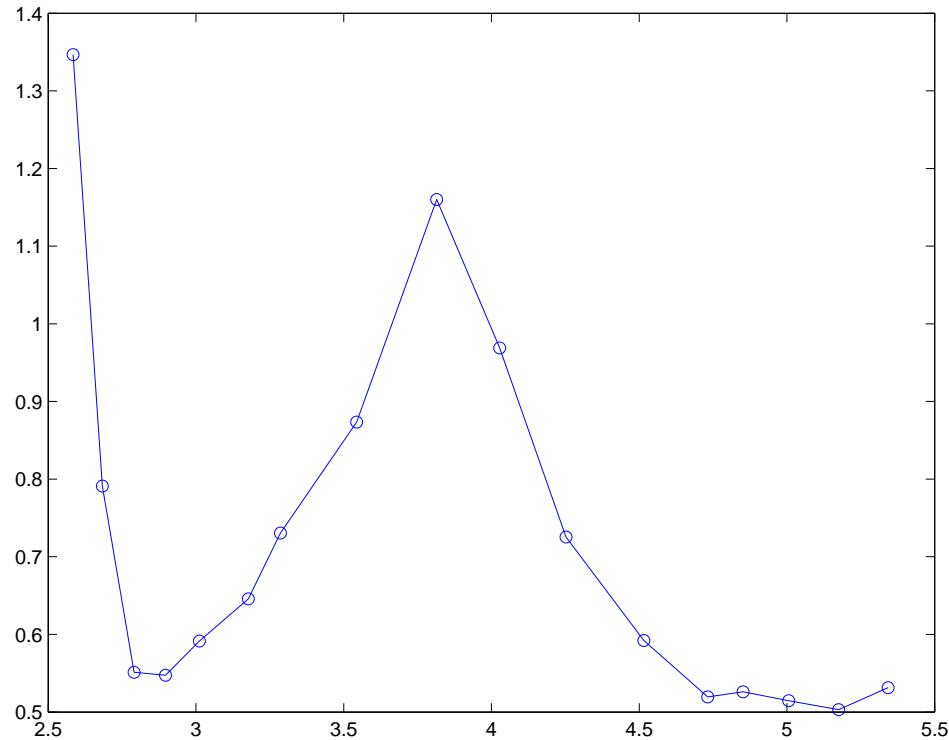
$$(R(\hat{U}), \hat{v}) + (hR(\hat{U}), R(\hat{v})) = 0 \quad \forall \hat{v} \in \hat{V}_h$$

Energy estimate for G2 (assuming  $f = 0$ ): set  $\hat{v} = \hat{U}$

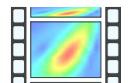
$$\frac{1}{2} \|U(t)\|^2 + \|\sqrt{\nu} \nabla U\|_Q^2 + \|\sqrt{h} R(\hat{U})\|_Q^2 = \frac{1}{2} \|U(0)\|^2$$

Total dissipation of energy:  $\|\sqrt{\nu} \nabla U\|_Q^2 + \|\sqrt{h} R(\hat{U})\|_Q^2$

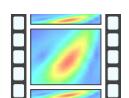
# Law of Finite Energy Dissipation



Flow around cube:



$Re=40\ 000: xy$



$Re=40\ 000: xz$

The intensity of the stabilizing term  $\|\sqrt{h}R(\hat{U})\|_Q^2$  in the wake is independent of  $h$  after some mesh refinement.